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THE USE OF OPAQUE LOUVRES AND SHIELDS TO REDUCE REFLECTIONS
WITHIN THE COCKPIT: COMPUTER PROGRAMS FOR TWO APPROACHES TO THE PROBLEM

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Final Report

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shield on top of the instrument panel to the more experimental use of Light			
Control Film ^R and Micromesh ^R for this purpose. Previous work in this series			
has demonstrated two mathematical approaches to a specific reflection pro-			
blem in the AH-1 aircraft, namely, the reflections coming from the portion			
of canopy directly above the gunner's head. It was felt that it would be use-			
ful to demonstrate the compatibility of these two approaches and to publish			

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SUMMARY

Opaque shields can be used to channel light and thereby reduce reflections within the cockpit. These shielding devices range from the standard glare shield on top of the instrument panel to the more experimental use of Light Control Film^R and Micromesh^R for this purpose. Previous work in this series has demonstrated two mathematical approaches to a specific reflection problem in the AH-l aircraft, namely, the reflections coming from the portion of canopy directly above the gunner's head. It was felt that it would be useful to demonstrate the compatibility of these two approaches and to publish the computer programs (FORTRAN) for each approach for possible use by others.

ROBERT W. BAILEY COL, MSC

Commanding

INTRODUCTION

One technique of reducing the reflections of the instruments, dials, etc. from the transparent enclosures is the use of opaque louvres and shields. In using these screening materials, one wants to maximize the extent to which they block light from reaching the canopy but minimize the extent to which they block light from reaching the pilots' eyes. This is accomplished by choosing the proper values for the position, width, spacing, angle, etc. of these shields.

In a previous report¹ we showed a set of mathematical equations for the solution of this problem in terms of analytic geometry. Quite independently, the problem has also been investigated by a different mathematical method, namely a plane geometrical and trigonometrical method. The latter method will be documented elsewhere². Regardless of the different mathematical derivations, results from these two theoretical predictions of the reduction in interior cockpit reflections were essentially identical. The purposes of this report are to demonstrate the compatibility of these two theoretical predictions and to document these two FORTRAN computer programs.

ANALYSIS

Due to the nature of the problem, visibility has been classified

into three cases. We denoted the projected points of the lower and higher points of the louvre to the vertical axis of the pilot's position by h and H respectively. Case I concerns the visibility \mathbf{V}_{I} above H. Visibility \mathbf{V}_{I} (Case II) is the region between H and h. Below h, visibility \mathbf{V}_{I} is classified as Case III. Since Case II is relatively III trivial and since Case III is similar to Case I, we will show the equations for Case I by these two methods.

a. Analytical geometry method:

$$V_{I_A} = 1 \frac{d_1}{c} \frac{\tan \Theta - k_1}{1 + k_1 \tan \Theta}$$
 (A)

Where V_{I_A} is visibility, c is the distance between louvres, d_1 is the thickness of the louvre, Θ is the decline angle of the instrument panel and k_1 is constant. All the symbols were explained in the original paper and are shown in Appendix I (incorporated with notations in the computer programs).

b. Plane geometrical method:

$$V_{I_{B}} = K \frac{1 (h-H) (Cot^{\alpha} Cos \Theta + Sin \Theta)}{h sec (\alpha-\Theta) - 1 - \alpha sin \Theta sec (\alpha-\Theta) - (h-H Cos \Theta Sin \alpha) (B)}$$

Where V is visibility, K is constant, h is the minimum height, H is the maximum height, Θ is the decline angle of the instrument panel and α is the extended angle.

A detailed explanation of the symbols in this equation is also given in Appendix II.

SOLUTION

Computer programs for equations (A) and (B) are attached in Appendices III and IV respectively. Comments and notations used have been added in the programs except for the graphic portion of the programs, which required a few calls from standard subroutines, and were plotted through a hybrid computer plotter³.

Results from both methods have been represented by two graphs (Figures 1 and 2 correspond to methods (A) and (B) respectively.). They were indistinguishably identical. (The vertical axis showed the normalized visibility and the horizontal axis was the vertical distance with respect to a referenced ground point in the Cartesian coordinates system. There are six curves in each graph with each curve representing a different louvre width. These graphic representations enabled us to determine the amount of visibility of a pilot under a set of predetermined cockpit parameters.

In short, this study has presented two different mathematical formulations which produced identical solutions for the analysis of the use of opaque louvres and shields to reduce reflections within the cockpit. It has also documented two computational procedures with their respective computer programs for future analyses of cockpit light reflections.

CONCLUSION

Previous work in this series has demonstrated two mathematical approaches to a specific reflection problem, namely, the reflections coming from the portion of canopy directly above the gunner's head. Although these two studies addressed a specific reflection problem, they each represented the modulus of a general approach to the canopy reflection problem. Therefore, it was felt that it would be useful to demonstrate the compatibility of these two approaches and to publish the computer programs for each approach for possible use by others.

RECOMMENDATIONS

In future canopy design, it is recommended that an analysis of this sort be carried out prior to fabrication of the canopy and cockpit. In this way, some potential reflection problems could be prevented without having to initiate costly re-designs and product improvement programs.

REFERENCES

- 1. Chiou, W.C. and Holly, F.F., "The Use of Opaque Louvres and Shields to Reduce Reflections Within the Cockpit: A Mathematical Treatment", USAARL Report NO. 75-22, June 1975.
- Park, C.K. and Holly, F.F., "The Use of Opaque Louvres and Shields
 To Reduce Reflections Within the Cockpit: A Trigonometrical
 and Plane Geometrical Approach," USAARL Report NO. 76-4, Sep 75.
- 3. We thank Dr. H.D. Jones of the Hybrid Computer and Analysis Branch, USAARL, for establishing the plot portion of the computer programs.

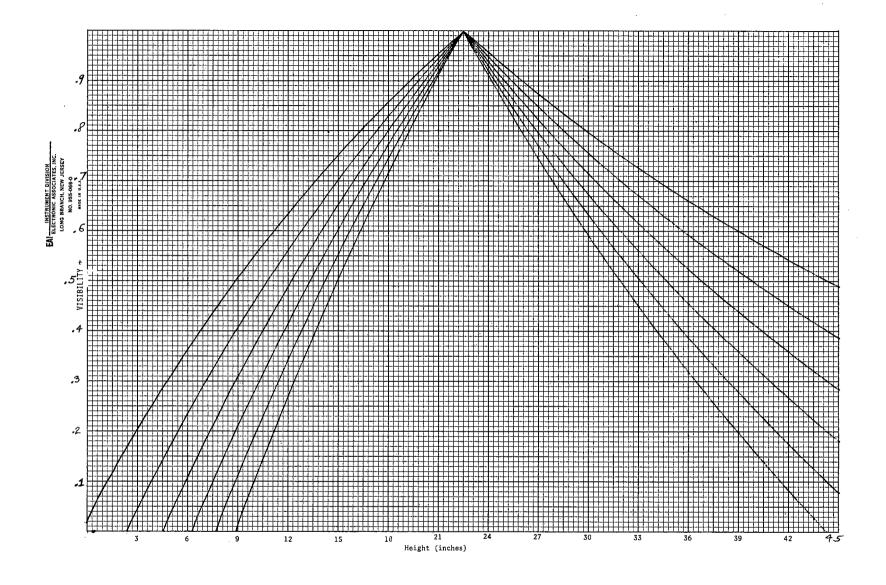


FIGURE 1. Visibility as a function of height in the plane of the gunner as determined by the method of analytic geometry.

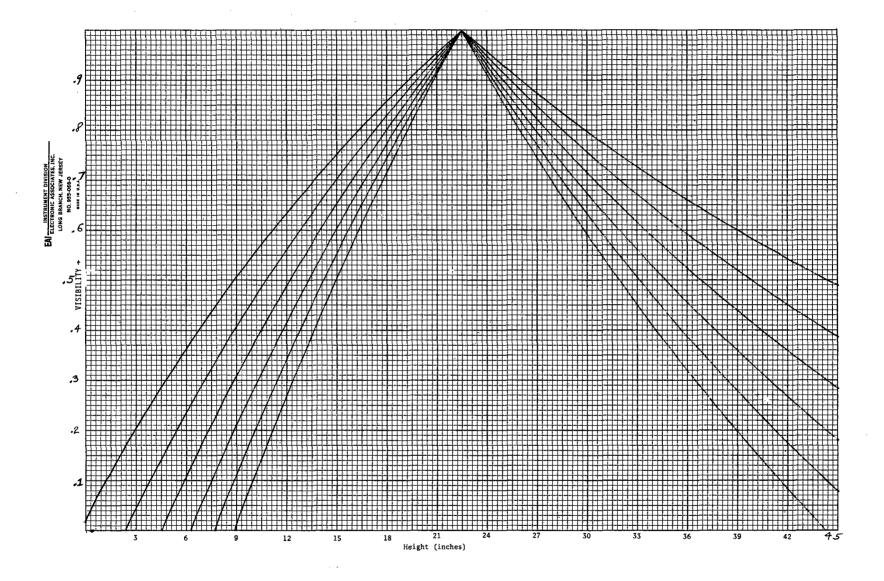


FIGURE 2. Visibility as a function of height in the plane of the gunner as determined by the method of plane geometry.

APPENDIX I
ANALYTICAL GEOMETRY METHOD

COL. (4 Decimal)	INPUT CODE	SYMBOLIC CODE	H E ADER CODE	COMMENT
1-7	Α	· a	A	Distance from panel
8-14	В .	b	. В	Distance the louvre is up the panel
19-21	С	С	C	Distance between the louvres
22-28	. D	· d ₁	D	Width of louvre
29-35	D ₂	d ₂	D ₂	Width of louvre
36-42	Е	Θ	E	LΘ
43-49	ORGN		ORGN	Beginning point

APPENDIX II
PLANE GEOMETRIC METHOD

COL (3 Decimal)	INPUT CODE	SYMBOLIC CODE	HEADER CODE	COMMENT
1-7	A	L .	L	Starting width of louvre Program Increments dy .003
8-14	В	α	В	Lα
15-21	c	K	K	Distance between louvres
22-28	. D	н	HF	Starting height to be varied \pm 10 by .25
29-35	Е	a	Α	Height up the panel
36-42	F	Θ	Т	LΘ
43-49	G	M	. M .	Distance from panel

APPENDIX III

COMPUTER PROGRAM (a)

		
75 76	VIV(I)=VII GO IO 500	
$\frac{15}{77}$	400 CONTINUE	
78	IF (PY(I) -GT -HY) 60 T0 500	
70	60 TO 600	· · · · · · · · · · · · · · · · · · ·
80	500 ČÕMĪIMĖŠ	•
8]	KA=A+ (H+C) #COS (E4)-D]#SIN(FA)
32	Kβ≡PY([]=((Ř+Č)#S[∿(FΔ)+π)	*COS(FA))
нз	K1=KA/K4	•
84		-K1)/(1+K1*SIN(FA)/COS(FA))
85	$VI \lor (I) = VI$	•
86	600 CO ITI dif	
97 88	TALL AND THE CONTRACT OF THE C	
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φ̈́)	5 CONTINUE	
څړن	C YS THIS IS PART OF SUBLING	
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94	00 23 M=1•8000	
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97	IAT=ICOTA*A(A(a)	
- 98	(2) 00 (H) 19 45 (45)	
99 100	51 COMTIME 229 IF(.WOT.M.FO.1.OR.W.FO.200	3100 Ta 555
107	<u> </u>	(1.4) 11(7.3)
105	7 FORMAT(! 1.14.5X.F(J.2.F)?	4)
103	232 CONTINE	• '/
104	C WRITING TO THE SAL & TO THE !	THE PRINTER TAKES PLACE IN THE FOLLOWING
105	CALL (BD4(0.1.101.101.16)	
106	## (M. #0. 1) Pange Pak	
107	23 CONTINUE	
108	9 WRITE (6.7) M. PY (M) . VIV (M)	
100	PAUSE LABEL	
110	90 TO 2 3 CONTINE	
111	STOP	
113	FWD	
114	SASSIGNI LIRETYNI I TO THE THITE	
115	\$4\$\$1692 5=\$YC	
117	\$4551GN2 6=510.7000	
117	SALLOCATE LOGOD	
ija	BOPTION MOMAS	
119	SEXECUTE GO	•
150	27.0.5.001015015.55.0.0	
121	27.0.5.0.01.012.012.512.55.0.0.0	
155	<u>~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~</u>	
123	27.0.2.0.01024024.55.0.0.0	
124	27.0.5.0.01.027.027.55.0.0.0	
125	27.0,5.0,0.01030030,55.0,0.9	•
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APPENDIX IV COMPUTER PROGRAM (b)

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                              AAH1 DR. HOLLY AND ES PARK
        SJOB.
         SOPTION
        SOPTION NOMAP
        FORTRAN
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        <del>32</del>
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<u>34</u>
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36
<del>37</del>
38
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43
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4 1
49
50
51
52
        IF (A) 3.4.4
4 CONTINUE
C*****************
                       * THE BIG DO LOOE INCREMENTS "A" THE WIDTH OF THE LOUVE.. THIS WILL PRAW THE DIFFERENT CURVES..THE LITTLE DO LOOF DRAWS THE CURVE IT SELF.. TOGETHER THEY WILL DRAW 6.
54
55
        Ĉ
56
57
58
                DO 20 J=1.6
            Y=0

K=0

PLUS=(C+E)*SIN(F)+A*SIN(B-F)

TAN=SIN(B-F)/COS(B-F)*(G+(C+E)*COS(F)-A*COS(B-F))

H=THE HEIGHT AT WHICH VISIBILITY IS 100%
60
61
62
63
        С
                 HEPLUSTAN
65
                D=H-20
        0.1 \pm 0
66
67
68
70
77
77
73
74
            DO 23 M=N,2000

IF (M)33,55,55

33 CONTINUE

THESE ARE SET UP IN MY FQUATION FOR UVII

DIV=A*(H=D)*(COS(B)/SIN(B)*COS(F)+SIN(F)

OIVER=H*1/SIN(B-F)-A-E*SIN(F)*1/SIN(B-F)

DIVER2=(D-H)*COS(F)*SIN(B)
        С
```

```
= THE VISIBLE PORTION RELOW THE LOUVRF ...

V=C-DIV/(DIVER+DIVER2)

GO. TO 66

CONTINUE

ESE ARE SET UP IN MY EQUATION FOR UVU

DIVER*(D-H)*COS(B-F)

DIVER*(D-H)*COS(B-F)

DIVER*(SF)*(F)*(G+K)*(COS(F)*A*COS(R-F))

= THE VISIBLE PORTION ABOVE THE LOUVPF ...

V=C-DIV/(DIVER+DIVER2)

CONTINUE

IF (V.GE.O) K=K+1

1 & IVI ARE MY X & Y IN SCALE FRACTION FORM FOR GRAPHING ID1=ICONV*(D-D1)/40.01

IVI=ICONV*(D-D1)/40.01

IVI=ICONV*(D-D1)/40.01
     75
                             C
    7<u>5</u>
77
78
    80
     82
     83
                             С
    84
85
86
    87
88
89
   90
91
92
                             Ċ
                             C
    94
95
    96
97
    <del>98</del>
99
100
101
102
103
                                     229
232
104
105
                                                      CONTINUE
                             \frac{106}{107}
 îŭė
                                                      D=D-.01
 <u> 109</u>
                                                      CONTINUE
                             D CUNITIUE
WRITE(6,230)D,V,M
CALL DELAY
CALL PENUP
20 A=A+.003
\frac{110}{111}
112
113
114
114
115
116
117
118
120
121
123
124
125
127
                             GO TO 2

3 CONTINUE

230 FORMAT('0',' X=D=HIGH= ',F9.4.lnx.'Y=V=VISIBLE= ',F9.4.4x.I6)

STOP
                            128
129
                                                    RETURN
ENTRY PENDOWN
CALL SSCL(15*IERR)
GO TO 2
ENTRY DELAY
DO 3 N=1*300000
X=0
RETURN
ENTRY DELAY2
DO 4 N=1*20000
 <del>130</del>
131
132
133
134
135
136
137
138
139
                                             3
                            141
142
143
144
145
<del>146</del>
147
148
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